

METHOD AND DEVICE FOR DETERMINATION OF THE CONDITION OF A
TURBINE BLADE, AND UTILIZING THE COLLECTED INFORMATION FOR
ESTIMATION OF THE LIFETIME OF THE BLADE

This invention regards a method of determining the condition
5 of a turbine blade and utilizing the collected information in
an estimation of the lifetime of the turbine blade. In
particular, it regards a method of determining when the
turbine blade is subjected to an undesirable condition, e.g.
in the form of so-called "rotating stall", whereupon the
10 measured and processed information is used as part of the
input information into a lifetime estimation programme. The
invention also regards a device for implementation of the
invention.

In this context, the condition of a turbine blade means the
15 type of loading to which the turbine blade is subjected. The
condition (operating state) may for example be normal
operation, rotating stall, etc.

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The estimation of the lifetime of a turbine blade, whereby the remaining lifetime may be determined, is of great importance in the planning of maintenance intervals. Prior methods of estimation were based exclusively on operating
5 time, as the lifetime of a turbine blade was set to an operating time during which it could, with reasonable certainty, be assumed that the turbine blade would exhibit satisfactory operation regardless of the loading exposed to the turbine blade during the operating time.

10 Obviously, such relatively simple lifetime estimation led to excessively frequent maintenance intervals, and the thus subsequent replacement of turbine blades that had been subjected to relative small loads during their operating time. Prior art now comprises lifetime estimation methods
15 that to some extent are quite complicated, in which parameters such as power loading, failures in both the component being monitored and in nearby components, wear, and also faults in the measuring equipment used to measure the loading, are taken into account in addition to operating
20 time.

For a turbine blade in a multi-stage axial compressor, it has been proven that rotating stall may cause overloading of the turbine blade with subsequent damage and compressor break-
25 down, without the condition being detected by equipment and methods according to prior art. Rotating stall can occur in a turbine stage when the air approaches the turbine blade at the wrong angle. This may cause the flow to separate in the boundary layer between blade and air (boundary separation), whereby a varying flow is generated at one or more locations
30 along the periphery of the stage. When a first turbine blade

is subjected to this condition, the air flow is deflected towards a nearby turbine blade, which is then overloaded while the other nearby turbine blade is relieved. This causes the overloaded turbine blade to be subjected to stall, whereby the first turbine blade is relieved. Thus rotating stall propagates along the periphery of the stage at a speed of approximately half the speed of rotation of the turbine.

According to prior art the compressor is monitored by measuring its performance. The measured values resulting from the measurements form part of the input values in a lifetime estimation tool. The measurements are compared with anticipated values, as the anticipated lifetime of the component in question or the entire turbine is affected by whether the measured value is greater or smaller than an anticipated value. However, this form of monitoring is not designed to allow determination of which compressor stage is being subjected to stall.

The object of the invention is to remedy the disadvantages of prior art.

The object is achieved in accordance with the invention, by the characteristics given in the description below and in the appended claims.

Trials have shown that representative and reliable measurement values that indicate the condition of the turbine blade may be obtained by means of a vibration sensitive sensor in the form of an accelerometer or other vibration sensitive instrument mounted on the turbine casing. The

sensor is mounted at or in relative proximity to the compressor stage(s) to be monitored.

Mounting the sensor on the outside of the compressor casing makes it unnecessary to provide through bores in the compressor casing, such as is common in connection with pressure measurements. In a compressor casing for e.g. an air craft, it is not practicable to drill the casing after certification.

The sensor picks up acoustically generated pressure waves from the turbine blades by the pressure waves propagating through the air to the compressor casing, causing the compressor casing to vibrate.

The measurement signal from the sensor is processed e.g. by means of so-called "Fast Fourier Transform" (FFT), in which the measurement signal is converted into measured values corresponding to those frequencies at which they normally occur, and by means of other signal processing filters that are known *per se*.

Measured values from several compressor stages where the stages have the same number of turbine blades, may if so desired be combined into one common set of measured values/measurements.

The measured values distributed over a frequency range are then compared with anticipated values at each of the corresponding frequencies. If the measured value at a frequency exceeds or falls below a predetermined measurement interval, a signal of the measured value is transmitted to a

lifetime estimation device, and the estimated lifetime is corrected in order to take into account the condition of the turbine blade in question.

In the boundary area between normal operation and rotating stall, the blade pass frequency of the compressor stage will be somewhat unstable and will fluctuate. By stating limits for the fluctuation, this condition can also be included in the lifetime estimation.

As mentioned above, rotating stall will propagate around the rotor at a speed of approximately half (50 to 70%) the speed of rotation of the turbine. The vibration energy generated by the rotating stall may be used as additional information in the lifetime estimation. However, the vibrational energy generated may be too low to be used as an indicator if rotating stall is occurring in one compressor stage only.

The following describes a non-limiting example of a preferred method and device illustrated in the accompanying drawings, in which:

Figure 1 shows an axial section through a compressor; and

Figure 2 shows a simplified diagram representing the analysis of the measured values.

In the drawings, reference number 1 denotes a section of a compressor comprising several compressor stages 2 with associated stator stages 4, compressor casing 6 and rotor 8.

On the compressor casing 6 there is placed a vibration sensitive sensor 10 connected via an electric line 11 to a signal processing device (not shown) of a type that is known *per se*.

- 5 After the signals from the sensor 10 have been processed in the signal processing device (not shown), they may be presented graphically as a diagram 12, see figure 2.

The frequency range in question is distributed along the abscissa 16 of the diagram, while the ordinate 18 of the
10 diagram 12 indicates the measured values. The processed signal is displayed as a curve 20.

Within a frequency range defined by line 22, the so-called "high pass" limit, and by line 24, the so-called "low pass" limit, in the diagram 12, a lower limit 26 and an upper limit
15 28 have been determined on the basis of empirical values, within which the peak level 30 of the curve 20 in said frequency range is located during normal operation.

Were a situation to occur in the compressor stage 2 in question, in which the air supply becomes too small, the
20 value of the peak level 30 will fall below value 26. This condition is communicated to the unit estimating the lifetime of the component. Similarly, if rotating stall were to occur, the peak value 30 would rise to a level higher than value 28, whereby a report on this condition is communicated to the
25 lifetime estimation device.

The abscissa 12 of the diagram may be divided into as many frequency ranges as required, with individual limit values

for each range. Typically, compressor stages with different numbers of turbine blades have separate frequency ranges, as the turbine blade pass frequency, which is equal to the speed of rotation multiplied by the number of blades, is different, s thereby occurring at different abscissa positions in the diagram 12.